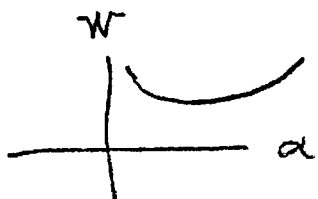


Then $\frac{d^2}{d\alpha^2} W(\underline{F}_0 + \alpha \underline{A}) = \frac{d}{d\alpha} \left(\frac{dW}{d\underline{F}}(\underline{F}_0 + \alpha \underline{A}) \cdot \underline{A} \right)$
 positive 2nd derivative!



$$= \underline{A} \cdot \frac{d^2 W}{d\underline{F}^2}(\underline{F}_0 + \alpha \underline{A}) [\underline{A}] > 0$$

from (*),

$\Rightarrow \alpha \mapsto W(\underline{F}_0 + \alpha \underline{A})$ is convex - which is (can be shown) equivalent to convexity of $W(\underline{F})$ (p. 93).

On the other hand, (SE) also implies a kind of convexity, but only in "rank-one" directions, i.e., only "rank-one excursions" from a given \underline{F}_0 are allowed: $\underline{F}_0 + \alpha \underline{a} \otimes \underline{b}$

$\underline{a}, \underline{b} \neq \underline{0}$

Then $\frac{d}{d\alpha} W(\underline{F}_0 + \alpha \underline{a} \otimes \underline{b}) \Big|_{\alpha=0} = \underline{a} \otimes \underline{b} \cdot \frac{dW}{d\underline{F}}(\underline{F}_0)$

$= \tilde{S}_{\alpha\beta}(\underline{F}_0)$ comp. 1st PK

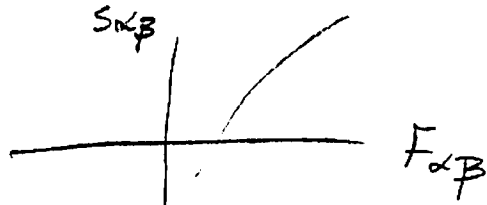
Also $\frac{d^2}{d\alpha^2} W(\underline{F}_0 + \alpha \underline{a} \otimes \underline{b}) \Big|_{\alpha=0}$

$= \frac{d}{d\alpha} \left[\frac{dW}{d\underline{F}}(\underline{F}_0 + \alpha \underline{a} \otimes \underline{b}) \cdot \underline{a} \otimes \underline{b} \right] \Big|_{\alpha=0}$

$\equiv \frac{d \tilde{S}_{\alpha\beta}(\underline{F}_0)}{dF_{\alpha\beta}} = \underline{a} \otimes \underline{b} \cdot \underline{C}(\underline{F}_0) [\underline{a} \otimes \underline{b}] > 0$

This is physically appealing: observe that $\alpha \underline{a} \otimes \underline{a}$ represents an extension along \underline{a} , while $\alpha \underline{e}_1 \otimes \underline{e}_2$ " a shear. (SE) \Rightarrow

$$\frac{d\tilde{S}_{\alpha\beta}(F_0)}{dF_{\alpha\beta}} > 0 \quad \text{rank-one monotone increasing}$$



$$S_{\alpha\beta} \equiv \underline{a} \otimes \underline{b} \cdot \underline{S} = \underline{a} \cdot \underline{S} \underline{b}$$

$$F_{\alpha\beta} \equiv \underline{a} \otimes \underline{b} \cdot \underline{F} = \underline{a} \cdot \underline{F} \underline{b}$$

We remark that, as the name suggests, (SE) \Rightarrow static bvp (p.104) is elliptic. In particular, the linearized static problem (p.111 with $w_t = w_{tt} \equiv 0$) is a well-posed linear elliptic pde - subject to the Fredholm alternative, i.e., non uniqueness is allowed (bifurcation)!

Verifying (SE) for specific material is not an easy task. For the Green-Nadaman material (p.73), it can be shown that $a > 0$, $b \geq 0$ and $\Pi''(J) \geq 0 \quad \forall J \Rightarrow$ (SE).

Caution Returning to the results of Exercise
 (17), suppose that we assume that

$\frac{d^2\psi}{dE^2}(E)$ is positive definite. Observe

$$\begin{aligned} \text{that } \underline{a} \otimes \underline{b} \cdot \underline{C}(E) [\underline{a} \otimes \underline{b}] \\ &= \underline{a} \otimes \underline{b} \cdot \left(\underline{a} \otimes \underline{b} \frac{d\psi}{dE}(E) \right) \\ &\quad + \underline{a} \otimes \underline{b} \cdot \underline{F} \frac{d^2\psi}{dE^2}(E) \left[\frac{1}{2} (\underline{F}^T (\underline{a} \otimes \underline{b}) \right. \\ &\quad \left. + (\underline{b} \otimes \underline{a}) \underline{E}) \right] \end{aligned}$$

Clearly, we have no "control" over $\frac{d\psi}{dE}(E)$

\Rightarrow ellipticity can fail!

To finish this part on the 3-dimensional theory, we return to the calculus of variations to briefly discuss the work of John Ball. Recall the Green-Hadamard material:

$$(*) \quad W(\underline{\underline{F}}) = a \underline{\underline{F}} \cdot \underline{\underline{F}} + b \operatorname{Cof} \underline{\underline{F}} \cdot \operatorname{Cof} \underline{\underline{F}} + \Gamma(\det \underline{\underline{F}}),$$

with $a > 0$, $b > 0$ and $\Gamma(\cdot)$ convex.

It turns out that $\underline{\underline{F}} \mapsto \operatorname{Cof} \underline{\underline{F}}$ and $\underline{\underline{F}} \mapsto \det \underline{\underline{F}}$ are not convex functions. Hence,

$\underline{\underline{F}} \mapsto W(\underline{\underline{F}})$ above (*) is not convex, which is good. On the other hand, $\underline{\underline{F}} \mapsto \underline{\underline{F}} \cdot \underline{\underline{F}}$,

$\underline{\underline{H}} \mapsto \underline{\underline{H}} \cdot \underline{\underline{H}}$ and $J \mapsto \Gamma(J)$ are each convex functions. Thus,

$(\underline{\underline{F}}, \underline{\underline{H}}, J) \mapsto a \underline{\underline{F}} \cdot \underline{\underline{F}} + b \underline{\underline{H}} \cdot \underline{\underline{H}} + \Gamma(J)$ is convex.

More generally, Ball considered

$$W(\underline{\underline{F}}) = \Phi(\underline{\underline{F}}, \operatorname{Cof} \underline{\underline{F}}, \det \underline{\underline{F}}),$$

with $W \rightarrow \infty$ as $|\underline{\underline{F}}| \rightarrow \infty$ (and/or $\det \underline{\underline{F}} \downarrow 0$),

where $(\underline{F}, \underline{H}, \underline{J}) \mapsto \underline{\Phi}(\underline{F}, \underline{H}, \underline{J})$ is convex. Such a function is said to be poly-convex. For a very general class of mixed boundary value problems (without assuming smoothness), Ball was able to show that [1977]

$$V[\underline{f}] = \int_B \underline{\Phi}(\underline{\nabla} \underline{f}, \text{Cof } \underline{\nabla} \underline{f}, \det \underline{\nabla} \underline{f}) dV + \text{cons.} \begin{cases} \text{body force} \\ \text{traction} \end{cases}$$

has a minimum \underline{f}^* (not necessarily unique) in $W^{1,p}(B)$ satisfying $\det \underline{\nabla} \underline{f}^* > 0$ a.e..

Moreover, polyconvexity \Rightarrow $\underline{a} \otimes \underline{b} \cdot \underline{\Phi}(\underline{F})[\underline{a} \otimes \underline{b}] \geq 0 \quad \forall \underline{a}, \underline{b} \neq 0$ not quite (SE)
 \Rightarrow rank-one convexity.

However, is \underline{f}^* a weak solution?

unknown - even for assumed smoothness

Because $\frac{d}{d\alpha} V(\underline{f}^* + \alpha \underline{u})|_{\alpha=0} (= 0)$ cannot be done rigorously

Special Cosset Theory of Rods

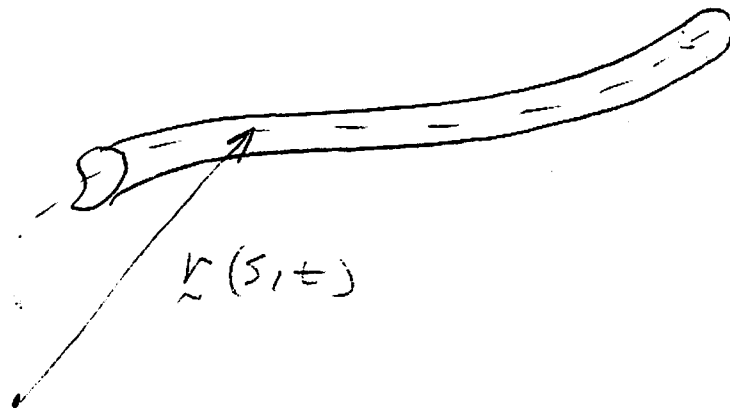
Roughly speaking, a rod is a "long, thin body" = L (length) \gg area of cross-section. There are two basic approaches:

- ① Direct approach: Treat rods as space curves with "micro-structure"
- ② Treat rods as constrained 3-d elastic bodies

We will freely "bounce between" these two approaches - although we will simply employ ② to motivate ① in the end.

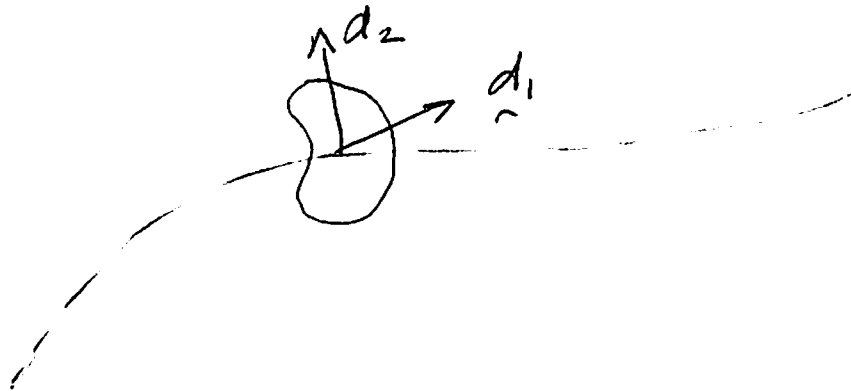
Some Preliminary Kinematics

Let $s \mapsto \underline{r}(s, t)$ denote the "centroidal" curve of a "slender" 3-dimensional body:

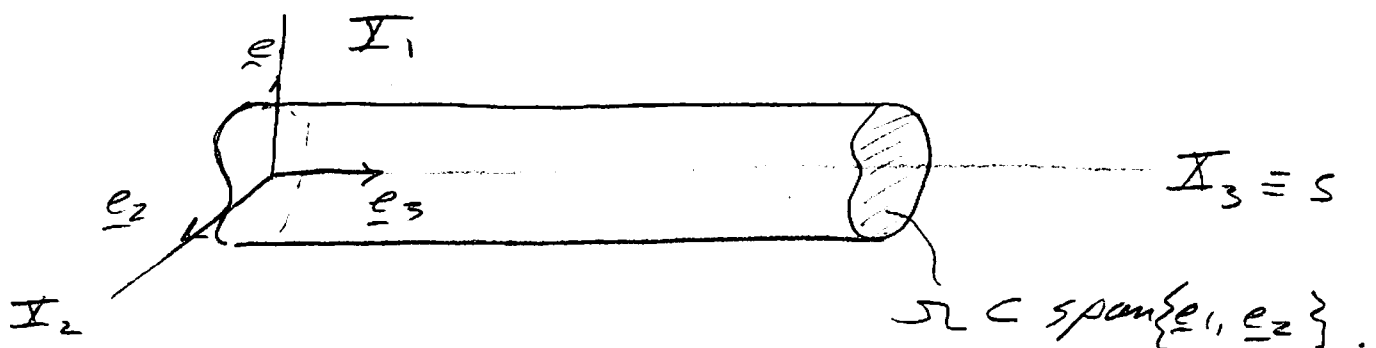


To model the cross-section, we attach to spanning vector fields $\underline{d}_1(s, t)$, $\underline{d}_2(s, t)$

at the centroid as (s, t) :



For simplicity, we assume a straight, prismatic reference configuration:



We choose "s" to be the arclength in the straight reference configuration. Since the $X_3 = s$ axis is centroidal, we have

$$\int_{\Omega} X_{\alpha} dA = 0, \quad \alpha = 1, 2.$$

Moreover, we choose \underline{e}_1 & \underline{e}_2 to be principal:

$$\int_{\Omega} X_1 X_2 dA = 0.$$

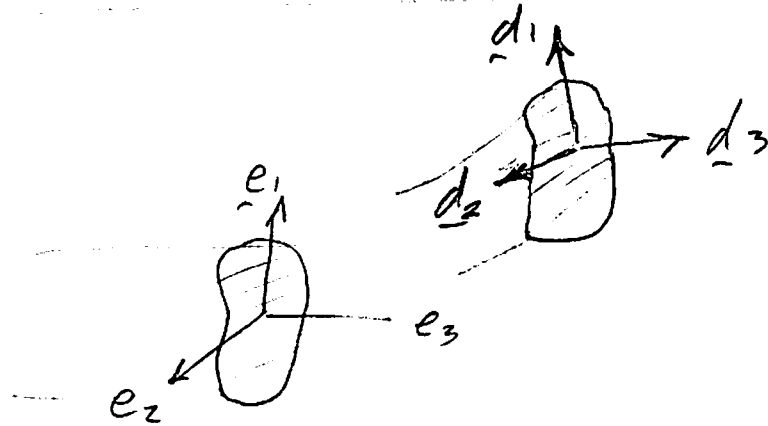
Defn: A deformation of a rod is a

mapping $s \mapsto \underline{r}(s), \underline{d}_\alpha(s), \alpha=1,2$. A motion of a rod is a one-parameter family of deformations $\underline{r}(s,t), \underline{d}_\alpha(s,t)$.

Motivation plane sections remain plane:

$$\underline{\underline{f}}(\underline{\underline{X}}) = \underline{r}(s) + \sum_{\alpha=1,2} \underline{I}_\alpha \underline{d}_\alpha(s) \quad (s = \underline{X}_3)$$

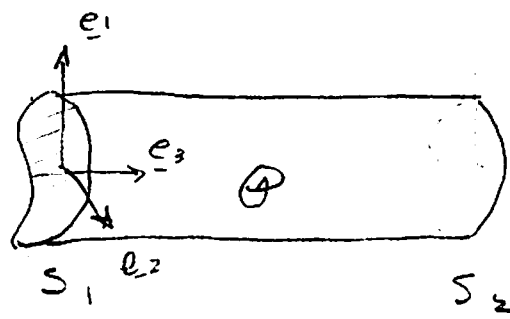
Gradients \rightarrow sum 1,2



We view $\underline{d}_1(s)$ & $\underline{d}_2(s)$ as spanning the plane of the deformed image of Ω . The vectors $\underline{d}_1(s)$ & $\underline{d}_2(s)$ are called directors.

Balance of Linear Momentum

Consider a segment of the straight, prismatic body:



Referring back to p. 28, we have

$$(*) \int_{\partial\Omega} \underline{\underline{S}} \underline{\underline{m}} \, dS + \int_{\Omega} \hat{\underline{\underline{b}}} \, dV = \int_{\Omega} \rho_0 \frac{d^2 \underline{\underline{f}}}{dt^2}$$

Now $\int_{\partial\Omega} \underline{\underline{S}} \underline{\underline{m}} \, dS =$ (3 parts)

$$\int_{\Omega} - \underline{\underline{S}}(\underline{\underline{x}}_1, \underline{\underline{x}}_2, s_1, t) \underline{\underline{e}}_3 \, dA + \int_{\Omega} \underline{\underline{S}}(\underline{\underline{x}}_1, \underline{\underline{x}}_2, s_2, t) \underline{\underline{e}}_3 \, dA$$

$$+ \int_{s_1}^{s_2} \oint_{\partial\Omega} \hat{\underline{\underline{A}}} \, dl \, ds \quad \leftarrow \text{imposed traction on lateral surface}$$

Also, $\int_{\Omega} \rho_0 \frac{d^2 \underline{\underline{f}}}{dt^2} \, dV = \int_{s_1}^{s_2} \int_{\Omega} \rho_0 \left(\underline{\underline{r}}_{tt} + \underline{\underline{x}} \cdot \underline{\underline{d}}_{\alpha, tt} \right) \, dA \, ds$
↙ $\underline{\underline{r}}_{tt}$ \leftarrow $\underline{\underline{r}}$ centrodial

Thus (*) leads

$$(**) \left(\int_{\Omega} \underline{\underline{S}} \underline{\underline{e}}_3 \, dA \right) \Big|_{s_1}^{s_2} + \int_{s_1}^{s_2} \left(\int_{\Omega} \hat{\underline{\underline{b}}} \, dA + \oint_{\partial\Omega} \hat{\underline{\underline{A}}} \, dl \right) \, ds$$

$$= \int_{s_1}^{s_2} \left(\int_{\Omega} \rho_0 \, dA \right) \underline{\underline{r}}_{tt}$$

Define $\underline{\underline{n}}(s, t) \equiv \int_{\Omega} \underline{\underline{S}}(\underline{\underline{x}}_1, \underline{\underline{x}}_2, s, t) \underline{\underline{e}}_3 \, dA$
 "true" contact force

$$\hat{\underline{b}}(s, t) \equiv \int_{\Omega} \hat{\underline{b}}_0 dA + \oint_{\partial\Omega} \hat{\underline{t}} dl$$

body force/unit length

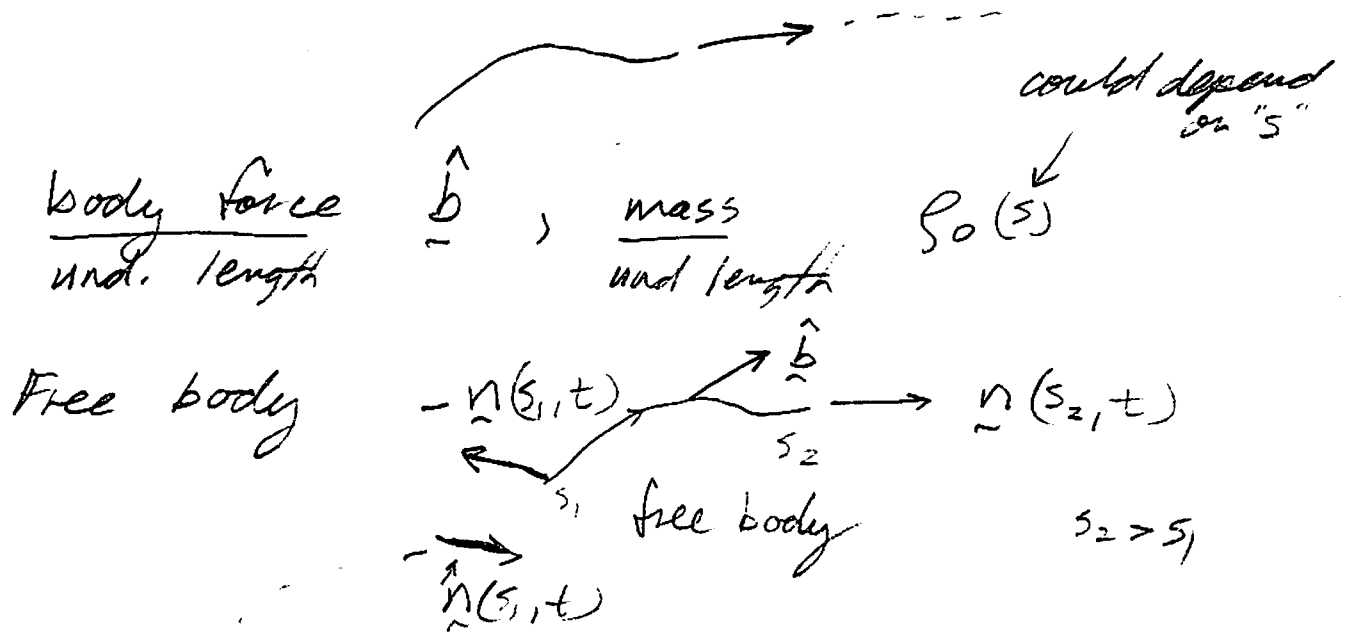
$$\rho_0(s) \equiv \int_{\Omega} \rho_0 dA$$

Then (***) leads:

$$\text{LMB} \quad \hat{\underline{n}} \Big|_{s_1}^{s_2} + \int_{s_1}^{s_2} \hat{\underline{b}} ds = \int_{s_1}^{s_2} \rho_0 \underline{r}_{tt} ds$$

Direct approach

Postulate: contact force $\hat{\underline{n}}(s, t)$, which represents the force at part \mathcal{P} at (s, t) due to contact with "external" world.



$$\begin{aligned} \text{LMB} \Rightarrow \quad \bar{n}(s_2, t) - \bar{n}(s_1, t) + \int_{s_1}^{s_2} \hat{\bar{b}} ds \\ = \frac{d}{dt} \int_{s_1}^{s_2} \rho_0 \bar{r}_t ds \quad \checkmark \end{aligned}$$

Local Form:

Observe $\bar{n} \Big|_{s_1}^{s_2} \overset{\text{Fund thm calc.}}{=} \int_{s_1}^{s_2} \bar{n}_s ds$

$$\Rightarrow \int_{s_1}^{s_2} (\bar{n}_s + \hat{\bar{b}} - \rho_0 \bar{r}_{tt}) ds = 0$$

$\forall (s_1, s_2)$ "parts"

Assuming continuity of integrand \Rightarrow

$$(*) \quad \boxed{\bar{n}_s + \hat{\bar{b}} = \rho_0 \bar{r}_{tt}}$$

Next we take the same approach to angular momentum balance: Referring back to our part \mathcal{P} on p. 123, we need the referential version of angular momentum balance:

$$\begin{aligned} \text{total moment } \bar{M}_d(\mathcal{P}) &= \int_{\partial \mathcal{P}} \bar{f} \times \bar{s}_m ds + \int_{\mathcal{P}} \bar{f} \times \hat{\bar{b}} dV \\ &= \frac{d}{dt} \bar{H}_0(\mathcal{P}), \end{aligned}$$